



08/701457

Transmitted herewith for filing is the patent application of

Inventor(s): Seiro YAHATA, Takanori ENDO, Masami MIYAKE and  
Takashi TSUCHIDA

For: **ANTENNA FOR TRANSPONDER AND TRANSPONDER**

XX Specification - 16 pages, Claims - 6 pages, Abstract - 1 page.

XX Drawings - 4 sheets of drawings.

Declaration and Power of Attorney  
not attached; deferred under P. L. 97-247.

A filing fee, calculated as shown below:

	Number Filed	Number Extra	Rate	Basic Fee \$750.00
Total Claims	35 - 20	15	x 22.00	330.00
Independent Claims	3 - 3	0	x 78.00	
Multiple Dependent Claims			250.00	
Reduction by 1/2 for small entity				
Fee for recording Assignment				40.00
<b>TOTAL</b>				<b>\$1120.00</b>

XX NO FEE ENCLOSED. THE FILING FEE IS DEFERRED.

Atty Docket No. 960630  
Suite 1000,  
1725 K. Street, N.W.  
Washington, D.C. 20006  
Tel: (202) 659-2930  
Fax: (202) 887-0357  
WFW/yap  
Enclosures: Spec.; Clms.; Abstr.; Draws. (4 sheets).

Respectfully Submitted,  
ARMSTRONG, WESTERMAN, HATTORI,  
McLELLAND & NAUGHTON

William F. Westerman  
Reg. No. 29,988



H

Almo fee

08/701457

# ANTENNA FOR TRANSPONDER AND TRANSPONDER

## FIELD OF THE INVENTION

*and antennas for use therewith*  
a The present invention relates to ~~antennas for transponders and to transponders~~. In  
a particular, the present invention relates to *an antenna* ~~an antenna for a transponder~~ and a transponder  
operating at a frequency of 40 kHz to 200 kHz, or at a frequency exceeding 100 kHz, which is  
suitable for the usage of an apparatus carried on a person, such as an ID card, a commuter pass  
and a coupon ticket.

## DESCRIPTION OF THE RELATED ART

*in the prior art*  
a Antennas which have previously been used include those of a winding on a ferrite  
magnetic core, and those of a wound conductor without a magnetic core. In antennas used in  
a *alternating* ~~alternate~~ magnetic fields, the use of the magnetic core comprising layered thin plates prevents  
a *losses resulting from* ~~a loss due to eddy currents~~

When a prior art antenna is used for transponders carried on persons for ID cards,  
a commuter passes and coupon tickets, the following problems arise:  
a Because ferrite is hard *and inflexible* ~~not flexible~~, and thus fragile against bending, it is not suitable  
a *sacket, shirt or pants* ~~for being carried in a pocket.~~

Although a coil not having a magnetic core can be made thin by forming a concentric  
a spiral coil 1 as shown in FIG. 2A, the coil characteristics are lowered when a coin 10 or the  
aluminum foil in a cigarette case in a person's pocket overlaps perpendicularly with the axis of

a a transponder 2 having such a coil 1 as shown in FIG. 2B. Such a characteristic deterioration can be prevented with significant inconvenience by taking the transponder out of the pocket when using it. Further, such a use may cause the deterioration of characteristics due to attached water drops or snow.

a When a metallic magnetic core is used with an ~~alternate~~ *alternating* current, the loss due to eddy ~~currents~~ *losses resulting from*  
a ~~currents have~~ *currents have* been prevented by layering thin magnetic plates having high electric resistance while  
a ~~insulating the plates from each other.~~ *one another* Such an effect is more ~~enhanced~~ *greatly* with a higher electric resistance and a smaller thickness of the magnetic material. However, at a frequency exceeding a few dozen kHz, and in particular, a few hundred kHz, a significant loss is ~~caused~~ *produced* and thus it is not suitable for use even if a material is used which has the highest electric resistance and the smallest thickness and is industrially available, i.e., an amorphous metal having an electric resistance of  $137 \mu\Omega\text{cm}$  and a thickness of  $23 \mu$ .

#### *SUMMARY* ~~OBJECT OF THE INVENTION~~

a It is an object of the present invention to provide an ~~antenna~~ *antenna* for a transponder and a  
a ~~transponder using thereof,~~ *transponder using thereof,* which is thin and flexible, has a ~~small~~ *low* loss at a high frequency, and  
a ~~is barely affected by a coin or an aluminum foil such as that used for cigarette packaging.~~ *insignificantly*

An antenna for a transponder in accordance with a first embodiment of the present invention comprises a magnetic core composed of layered rectangular metallic thin plates, and  
a a coil wound parallel to the ~~longer side~~ *a greater dimension* of the magnetic core.

Because the magnetic core in such an antenna for a transponder is composed of layered metallic thin plates, the antenna is thin and flexible, and has a decreased high-frequency loss.

By winding a coil in the longer side direction of the magnetic core, the loss is significantly decreased at a high frequency region over a few dozen kHz.

When the antenna for the transponder is mounted in a transponder, the magnetic flux flows parallel to the transponder's plane. Thus, the magnetic flux is barely affected by a coin or aluminum foil overlapped on the transponder's plane.

A transponder in accordance with a second embodiment of the present invention has two plate antennas each comprising a magnetic core composed of layered metallic thin plates wound with a conductor coil, and an air-core antenna composed of a spirally wound conductor.

An antenna for a transponder in accordance with a third embodiment of the present invention comprises a plate magnetic core composed of a composite material of a soft magnetic flake and a synthetic resin, and a coil wound on such a magnetic core.

Such an antenna for a transponder is thin and flexible and has a decreased high-frequency loss, because the magnetic core is composed of a composite material of <sup>such as</sup> a soft magnetic flake and a synthetic resin.

When the antenna for the transponder is fabricated in a transponder, the magnetic flux flows parallel to the transponder plate. Thus, the magnetic flux is barely affected by a coin or aluminum foil overlapped on the transponder plate.

A transponder in accordance with a fourth embodiment of the present invention comprises two plate antennas in accordance with the third embodiment set forth above, and an air-core antenna composed of a spirally wound conductor.

## BRIEF DESCRIPTION OF THE DRAWINGS

*a* FIG. 1 is an isometric view illustrating <sup>*a first*</sup> ~~an~~ antenna in accordance with an embodiment of the present invention;

FIG. 2A is a plan view illustrating a transponder having a prior art antenna and FIG. 2B is an isometric view of the same;

FIGs. 3A and 3B are plan views illustrating a magnetic core in accordance with an embodiment of the present invention;

FIG. 4A is a plan view illustrating a transponder in accordance with an embodiment of the present invention and FIG. 4B is an isometric view of the same;

FIG. 5A is a plan view illustrating a transponder also usable as a magnetic card and FIG. 5B is a side view of the same;

FIGs. 6A and 6B are representative views illustrating the length, width and thickness of coils in Example (6A) and Comparative Example (6B); and

FIG. 7A is a plan view illustrating a transponder in accordance with an embodiment of the present invention, and FIG. 7B is a side view of the same.

## DESCRIPTION OF THE PREFERRED EMBODIMENTS

*a* <sup>*A*</sup> ~~An antenna for a transponder,~~ <sup>*antenna*</sup> in accordance with a first embodiment of the present invention will now be explained.

FIG. 1 is an isometric view illustrating a preferable feature of an antenna in accordance with the first embodiment of the present invention.

This antenna comprises a magnetic core 4 composed of layered metallic thin plates, and

a coil 5 wound thereon.

Preferred materials for the metallic thin plate are soft magnetic materials, and in particular, of having excellent magnetic properties and a large specific resistance. Examples of such materials include amorphous magnetic materials, such as METAGLAS 2714A (Co-Fe-Ni-B-Si type), 2605S2 (Fe-B-Si type), 2605SC (Fe-B-Si-C type) and 2876MB (Fe-Ni-Mo-B type) made by Allied Signal; iron-nickel alloys, such as JIS 2531 PB PC; silicon steels, such as JIS 2553 Z6H and RC6HL GO9 SO9; and the like. Among them, Co-Fe-Ni-B-Si-type amorphous magnetic material is more preferred, and the preferable thickness of ~~the~~ <sup>each</sup> metallic thin plate ranges 20 to 50  $\mu\text{m}$ .

The number of the layered metallic thin plates is preferably 3 to 16. Although only metallic thin plates can be layered without inserting other material, metallic thin plates which are insulated by coating or oxidizing the surface of the plate also may be layered. Further, in order to secure the insulation between the metallic thin plates, an insulating material, such as paper and polymeric films may be inserted between the metallic thin plates in the layering.

The ratio B/A of the shorter side length B to the longer side length A in the magnetic core 4 composed of layered metallic thin plate is 1 or less, preferably 0.4 to 1.0 and more preferably 0.5 to 0.9.

The conductor wound up as the coil 5 is preferably 100 to 200  $\mu\text{m}$  in diameter. When the coil 5 is formed, the conductor is wound up in the direction parallel to <sup>a greater dimension</sup> the long side of the magnetic core 4. The preferable thickness of the antenna 3 after the coil is wound up is 0.4 mm or less, and ~~more~~ preferably 0.3 mm or less.

The cross-section of the conductor for the coil is typically circular, and is preferably

rectangular for the compact coil. The materials for the conductor are pure copper for general use, chromium copper (copper-base alloy containing chromium) for use requiring the strength due to vibration, highly conductive silver for compact size, corrosion resistive gold for use requiring high reliability, and aluminum for light weight.

The magnetic core of the antenna in accordance with the present invention is flexible in order to prevent breakage due to bending. Further, because the antenna is thin and the coil axis can be set to be parallel to the transponder plate, its characteristics are barely lowered when a coin or aluminum foil overlaps with the transponder. Thus, the antenna has a small loss at a high frequency.

In particular, when the corners of the magnetic core are *reduced to form oblique angles* ~~cut~~ or rounded as shown in FIGS. 3A and 3B and in Examples described after, the loss can be further suppressed at a high

frequency. The loss in the antenna in accordance with the present invention, of which the coil

is wound up with the magnetic core composed of layered metallic thin plates *parallel to a greater dimension* in the longer side direction, is significantly lowered at a high frequency region of a few dozen kHz, and the most

of the loss is generated at the corners of the magnetic core. Thus, the corners are *reduced to form oblique angles* ~~cut~~ or rounded

like a magnetic core 3A shown in FIG. 3A or core 3B shown in FIG. 3B, respectively, to decrease the loss.

When the corners are *reduced to form oblique angles* ~~cut~~, the length of the cut side (a in FIG. 3A) is generally 2 to 12 mm, preferably 3 to 10 mm, and more preferably 4 to 8 mm. When the corners are rounded, the curvature radius R is generally 2 to 15 mm, preferably 3 to 12 mm, and more preferably 4 to 10 mm.

*and antenna according to*  
Next, a transponder ~~of a second embodiment using the antenna in accordance with the~~

present invention will be explained.

The transponder in accordance with the present invention is produced by embedding the antenna 3 for the transponder, as well as a circuit chip, into a synthetic resin. The preferred size of the transponder is 54 mm in width and 86 mm in length, similar to credit cards generally used. A size <sup>greater</sup> ~~larger~~ than this is too bulky to carry, whereas a size less than this may often be lost, both resulting in inconvenient handling. The preferred thickness of the transponder is 0.76 mm or less, similar to credit cards.

As shown in FIGS. 4A and 4B, the plate transponder 8 in accordance with the present invention is provided with two thin plate antennas 6, 7, while their coil axes (or antenna axes) are perpendicular to <sup>one another</sup> ~~each other~~, and an air-core antenna composed of an air-core spiral coil 9 is provided in the transponder 8, so that the axis is perpendicular to the transponder plate. Axes of the antennas 6, 7 and of the antenna composed of the coil 9 are preferably directed in three directions perpendicular to each other. These antennas have chip circuits 11.

When the transponder is used as an ID card or a commuter pass for an automated wicket in a pocket, the transponder must respond to radio waves from any directions, because the correlation of the directions between the antenna of the interrogator and the transponder is not defined. Although the plate transponder can respond to all the directions parallel to the plate by providing two plate antennas which cross their axes, such a transponder cannot respond to the plane perpendicular to the plate. Further, the spiral antenna cannot respond to the direction parallel to the plate. On the other hand, the plate transponder shown in FIGs. 4A and 4B can respond to radio waves from all the directions, regardless of the direction of the transponder;



the antenna 7 responds to radio waves in the X direction, the antenna 6 responds to radio waves in the Y direction, and the air-core antenna (coil) 9 responds to radio waves in the ~~X~~<sup>Z</sup> direction.

The transponder 12 may be provided with a magnetic recording layer, such as a magnetic stripe 13, at the surface, and the antenna 14 in accordance with the present invention as shown in FIGs. 5A and 5B. The transponder can be used in both the contact and non-contact states. Any printing may be applied on the surface without magnetic recording for visual judgement. Any embossment can be formed at the sections other than the antenna, circuit and magnetic recording layer for clearer printing and improving the durability against rewrite and wear. The transponder 12 has a circuit chip 16.

An antenna for a transponder in accordance with a third embodiment will now be explained.

Examples of soft magnetic materials used for the flake of the antenna for the transponder in accordance with a third embodiment of the present invention include pure iron, silicon steel, permalloys (Fe-Ni alloy), iron/cobalt amorphous alloys, and in particular, cobalt amorphous alloys (Co-Fe-Ni-B-Si). Amorphous alloys have excellent high-frequency characteristics, and are readily formed to flakes by striking to quench the molten drops from the molten alloy flow on a copper surface cooled with water.

The thickness of the flake is preferably 30  $\mu\text{m}$  or less, and more preferably 10  $\mu\text{m}$  or less, to prevent the effect of eddy current. A larger flake diameter can increase the permeability of the composite material and decrease the magnetic core size. However, an excessively large diameter of the flake barely homogenizes the magnetic core material. Accordingly, flake diameter ranges 50 to 2,000  $\mu\text{m}$ , and preferably 100 to 1,000  $\mu\text{m}$ .

a Examples of synthetic resins include <sup>thermoset</sup> ~~thermoses~~ resins, e.g. epoxy resins, phenol resins, urea resins, unsaturated polyester resins, diacrylphthalate resins, melamine resins, silicone resins, and polyurethane resins; and thermoplastic resins, e.g. polyethylene resins, polypropylene resins, vinyl chloride resins, fluoroplastics, methacrylate resins, polystyrene resins, AS resins, ABS resins, ABA resins, polycarbonate resins, polyacetal resins, and polyimide resins.

The flexibility of the composite material increases and the shaping characteristics improves with the increased synthetic resin content in the composite material. When the resin content is too small, the strength of the composite material decreases. On the other hand, an excessive synthetic resin content causes a decrease in permeability. Accordingly, the preferable amount of the synthetic resin is 3 to 50 <sup>% by weight</sup> ~~weight%~~, and more preferably 10 to 40 <sup>% by weight</sup> ~~weight%~~ of the composite material.

Usable molding methods include injection molding, compression molding, rolling, and doctor blade shaping. A composite material having excellent magnetic characteristics can be obtained by compression molding, rolling or doctor blade shaping, since the flake plane is oriented to the plane of the composite material. The size suitable to carry is 0.3 to 2 mm in thickness, 100 mm or less in width and length, and in particular, 0.3 to 1 mm in thickness, 10 to 25 mm in width, and 60 to 80 mm in length.

When the conductor forming the coil is too thick, the antenna becomes too thick, whereas the excessively thin conductor causes an increase in resistance. Thus, the diameter of the conductor preferably ranges 100 to 200  $\mu\text{m}$ .

It is preferred that the coil is wound perpendicular to the longer side of the antenna, in other words, the coil axis is parallel to the longer side.

The antenna for the transponder in accordance with the present invention exhibits excellent effects in that the antenna is thin and flexible, the loss is low at a high frequency over 100 kHz, and the antenna is less affected by a coin or an aluminum foil package.

A transponder using an antenna in accordance with a fourth embodiment of the present invention will now be explained.

In this transponder, two plate antennas in accordance with the third embodiment are placed perpendicular to each other, and an air-core antenna composed of a spirally wound conductor is placed, similar to the second embodiment set forth above, because the direction of the transponder antenna is not always oriented in the direction of the magnetic flux of the reading machine when the transponder in a pocket passes through an automated wicket. As shown in FIGs. 7A and 7B, the two thin plate antennas 26, 27 in accordance with the present invention are provided in the plate transponder 28 so as to cross the axes of the coils or antennas of each other, and the air-core antenna composed of the air-core spiral coil 29 is provided in the plate transponder 28 so that the axis of the antenna is perpendicular to the plate of the transponder. Axes of the antennas 26, 27 and of the antenna composed of the coil 29 are preferably directed to three directions perpendicular to each other. These antennas have chip circuits 31.

When the transponder is used as an ID card or an automated wicket in the pocket, the correlation between the direction of the interrogator antenna and the direction of the transponder is not fixed. Thus, the transponder must respond to radio waves from all the directions. A transponder, which has two plate antennas crossing each other, can respond to the direction parallel to the plate, but cannot respond to the direction perpendicular to the plate. On the other

hand, the plate transponder shown in FIGs. 7A and 7B can respond to waves from all the directions, regardless the direction of the transponder; the antenna 27 responds to radio waves in the X direction, the antenna 26 responds to radio waves in the Y direction, and the air-core antenna (coil) 29 responds to radio waves in the <sup>Z</sup>~~X~~ direction.

### Experiment 1

A sheet composed of Allied Signal METAGLAS 2714A having a width of 50 mm and a thickness 25  $\mu$ m was used as a magnetic core material. The sheet was cut into a size shown in Table 1, was heated at 250°C for 10 min. in air, and quenched. A magnetic core was produced by layering a few sheets so as to reach the thickness shown in Table 1. An insulation conductor having a diameter of 0.15 mm was wound up on the magnetic core so that the L of the coil is approximately 3 mH. The conductor was wound in the direction parallel to the longer side of the magnetic core in Examples, and in the direction parallel to the shorter side of the magnetic core in Comparative Examples.

The resistance of each antenna due to the magnetic core was evaluated by the following equation from the resistance R obtained from Yokogawa-Hewlett-Packard LCR meter 4284A:

$$R_1 = R - R_2$$

wherein  $R_1$  represents a resistance due to the magnetic core, R represents an observed resistance, and  $R_2$  represents a direct current resistance of the coil.

Results are shown in Table 1. Table 1 demonstrates that the resistance significantly decreases by winding the coil in the direction parallel to the longer side of the magnetic core.

As shown in FIGs. 6A and 6B, the magnetic core size perpendicular to coil axis represents A, the magnetic core size parallel to coil axis represents B, and the magnetic core size perpendicular to the plane AB represents C.

### Experiment 2

A sheet composed of Allied Signal METAGLAS 2714A having a width of 50 mm and a thickness  $25\ \mu\text{m}$  was cut into 50 mm by 25 mm. Four corners of the cut sheet in Example A were cut as shown in FIG. 3A ( $a=6\ \text{mm}$ ). Four corners of the cut sheet in Example B were rounded as shown in FIG. 3B so as to form arcs ( $R=6\ \text{mm}$ ). Each corner in Example C was maintained to right angle. Sheets were heated at  $250^\circ\text{C}$  for 10 min. in air, and quenched. A magnetic core of each Example was produced by layering three sheets. An insulation conductor having a diameter of 0.15 mm was wound up twice by each 85 turns in the direction parallel to the longer side of the magnetic core to form an antenna. The direct current resistance of the coil was  $20.4\ \Omega$ .

The resistance of each antenna due to the magnetic core was evaluated similar to Experiment 1. Results are shown in Table 2. Table 2 demonstrates that the resistance significantly decreases by eliminating the corners of the magnetic core.

### Experiments 3

(Example)

A sheet composed of Allied Signal METAGLAS 2714A having a width of 50 mm and a thickness 0.025 mm was cut into 50 mm by 25 mm, heated at  $250^\circ\text{C}$  for 10 min. in air, and

quenched. A magnetic core was produced by layering three sheets. An insulation conductor having a diameter of 0.16 mm was wound up by 180 turns in the direction parallel to the longer side of the magnetic core.

(Comparative Example)

On the other hand, an antenna composed of an air-core coil of which a conductor having a diameter of 0.016 mm was wound to 400 turns.

(Measurement)

The resistance of the magnetic core of each sample, of which a 10-yen coin was placed in the coil center as shown in FIG. 2B, was measured similar to Experiments 1 and 2. Results are shown in Table 3. Table 3 demonstrates that the antenna of the Example exhibits a smaller resistance in a practical frequency region as a transponder of 40 to 200 kHz.

Experiment 4

(Examples)

No. 1

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of 5  $\mu\text{m}$  and an average diameter of 500  $\mu\text{m}$  with an epoxy resin in an amount of 10% (the rate of the resin to the total of the flake and resin) and by compression-molding at 160 °C and 200 kg/cm<sup>2</sup>. The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 2

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of  $5\text{ }\mu\text{m}$  and an average diameter of  $500\text{ }\mu\text{m}$  with an epoxy resin in an amount of 20% (the rate of the resin to the total of the flake and resin) and by compression-molding at  $160\text{ }^{\circ}\text{C}$  and  $200\text{ kg/cm}^2$ . The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 3

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of  $5\text{ }\mu\text{m}$  and an average diameter of  $500\text{ }\mu\text{m}$  with an epoxy resin in an amount of 30% (the rate of the resin to the total of the flake and resin) and by compression-molding at  $160\text{ }^{\circ}\text{C}$  and  $200\text{ kg/cm}^2$ . The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 4

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of  $5\text{ }\mu\text{m}$  and an average diameter of  $500\text{ }\mu\text{m}$  with an epoxy resin in an amount of 40% (the rate of the resin to the total of the flake and resin) and by compression-molding at  $160\text{ }^{\circ}\text{C}$  and  $200\text{ kg/cm}^2$ . The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor

having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 5

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of 5  $\mu\text{m}$  and an average diameter of 300  $\mu\text{m}$  with an epoxy resin in an amount of 20% (the rate of the resin to the total of the flake and resin) and by compression-molding at 160 °C and 200 kg/cm<sup>2</sup>. The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 6

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of 10  $\mu\text{m}$  and an average diameter of 500  $\mu\text{m}$  with an epoxy resin in an amount of 20% (the rate of the resin to the total of the flake and resin) and by compression-molding at 160 °C and 200 kg/cm<sup>2</sup>. The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

No. 7

A magnetic core material was prepared by mixing Co-type amorphous metal flakes having an average thickness of 5  $\mu\text{m}$  and an average diameter of 500  $\mu\text{m}$  with a mixture of a urethane resin and an epoxy resin in an amount of 20% (the rate of the resin mixture to the total



of the flake and resin mixture) and by compression-molding at 160°C and 200 kg/cm<sup>2</sup>. The magnetic core material was cut into cut sheets having a thickness of 0.6 mm, a width of 25 mm, and a length of 80 mm. A conductor having a diameter of 0.15 mm was wound in a direction parallel to the cut sheet so that L is 3 mH.

(Comparative Examples)

No. 1

A magnetic core material was prepared by cutting Allied Chemical METAGLAS 2714A into a rectangular pieces having a width of 25 mm and a length of 50 mm. A magnetic core having a thickness of 0.3 mm was produced by layering 12 pieces. A conductor having a diameter of 0.15 mm was wound in the direction parallel to the cut sheet so that L is 3 mH.

(Measurement)

The resistance R (loss) of each coil was measured with a Yokogawa-Hewlett-Packard LCR meter. Results are shown in Table 4.

Table 4 demonstrates that the antenna in accordance with the present invention exhibits a small loss in a high frequency region over 100 kHz.

(Table 1)

	Magnetic Core Size			Resistance due to Magnetic Core $R_i$ ( $\Omega$ )									
	A (mm)	B (mm)	C ( $\mu$ )	B/A	30 kHz	40 kHz	50 kHz	60 kHz	80 kHz	100 kHz	120 kHz	150 kHz	250 kHz
Examples	50	15	300	0.3	1.5	2.1	3.8	5.9	10.3	16.5	24.4	40.8	84.3
	50	20	300	0.4	2.3	4.1	5.8	8.5	14.7	23.0	26.4	48.2	98.8
	50	25	75	0.5	2.3	4.3	6.7	9.7	17.2	26.0	38.9	60.8	108
	50	25	150	0.5	2.4	4.8	7.3	10.1	17.5	26.8	37.8	56.2	106
	50	25	300	0.5	2.7	4.7	6.6	9.2	15.8	24.1	33.8	52.3	96.3
	50	25	600	0.5	2.7	4.8	6.4	8.6	14.9	23.5	32.4	49.6	92.3
	50	35	300	0.7	5.9	10.4	16	23.3	42.8	70.9	114	224	840
	50	50	300	1.0	9.9	17.7	28.2	41.6	77.5	134	224	480	2500
	50	75	300	1.5	10.8	25.1	38.0	80.7	103	162	281	816	4250
	50	100	300	2.0	12.7	28.8	48.9	72.5	115	194	335	910	5650
Comparative Examples	50	200	300	4.0	16.6	30.1	59.7	94.3	140	253	440	1030	7400

Remarks A: Magnetic core size perpendicular to coil axis

B: Magnetic core size parallel to coil axis

C: Thickness

(Table 2)

Frequency (kHz)	Example A Core with Cut Corner ( $\Omega$ )	Example B Core with Rounded Corner ( $\Omega$ )	Example C Core without Corner Treatment ( $\Omega$ )
30	2.1	2.2	2.7
40	3.7	3.8	4.4
50	3.5	3.7	4.8
60	5.7	6.0	7.8
80	13.9	14.5	17.6
100	23.7	24.7	29.4
120	37.7	39.2	46.6
150	54.1	56	65.8
200	108.6	112.3	134.1

502230-25470230

18

(Table 3)

Frequency ( kHz )	Example Coil with Core Core	Comparative Example Air-core Coil Conductor
	Diameter 0.16 mm Number of Turns 180 ( $\Omega$ )	Diameter 0.16 mm Number of Turns 400 ( $\Omega$ )
30	6.2	20.0
40	8.8	23.3
50	11.6	26.4
60	14.8	29.5
80	21.7	35.3
100	29.9	41.2
120	39.0	47.1
150	55.6	56.3
200	70.0	73.1

0070447 000000



WHAT IS CLAIMED IS:

Sub 97 1. An antenna for a transponder comprising a magnetic core composed of layered rectangular metallic thin plates, and a coil wound on said magnetic core parallel to longer side of said magnetic core.

2. An antenna for a transponder according to claim 1, wherein corners of said thin plate are cut or rounded.

3. An antenna for a transponder according to claim 1, wherein the thin plate comprises an amorphous magnetic material.

4. An antenna for a transponder according to claim 1, wherein the thickness of the thin plate is 20 to 50  $\mu\text{m}$ .

5. An antenna for a transponder according to claim 1, wherein the number of the layered thin plates is 3 to 16.

6. An antenna for a transponder according to claim 1, wherein the ratio B/A of the lengths of the shorter side B to the longer side A of the layered thin plates is 1 or less.

10  
7. An antenna for a transponder according to claim 6, wherein the ratio B/A of the lengths of the shorter side B to the longer side A of the layered thin plates is 0.4 to 1.0.

---

Sub 692  
8. An antenna for a transponder according to claim 1, wherein the thin plates are insulated by oxidizing their surfaces are layered.

---

9. An antenna for a transponder according to claim 1, wherein the diameter of the coil conductor is 100 to 200  $\mu\text{m}$ .

---

10. An antenna for a transponder according to claim 1, wherein the thickness of the antenna is 0.4 mm or less.

---

Sub 693  
11. An antenna for a transponder according to claim 1, wherein said antenna for a transponder is suitable to carry as an ID card, a commuter pass or a coupon ticket which operates at a frequency of 40 to 200 kHz.

---

12. A plate transponder comprising two plate antennas composed of a wound conductor on a magnetic core composed of layered metallic thin plates, and an air-core antenna composed of a spirally wound conductor.

---

13. A transponder according to claim 12, wherein axes of said three antennas are oriented to three directions perpendicular to each other.

---

Sub 94 14. A transponder according to claim 12, wherein said two plate antennas are provided in the plate transponder so that the axes of said two antennas or coils are perpendicular to each other, and said air-core antenna composed of the spirally wound conductor is provided in the plate transponder so that the axis thereof is perpendicular to the transponder Plate.

15. A transponder according to claim 12, wherein a magnetic recording layer such as a magnetic stripe is provided on the surface of the transponder, and antennas are provided inside the transponder.

16. A transponder according to claim 12, wherein printing is carried out on the surface.

Sub 95 17. A transponder according to claim 12, wherein embossment is formed on the sections other than said antennas, complimentary circuits, and a magnetic recording layer.

18. A transponder according to claim 12, wherein said transponder is suitable to carry as an ID card, a commuter pass or a coupon ticket which operates at a frequency of 40 to 200 kHz.

19. An antenna for a transponder comprising a plate magnetic core composed of a composite material of soft magnetic flakes and a synthetic resin, and a coil wound on said magnetic core.



20. An antenna for a transponder according to claim 19, wherein the soft magnetic material composing said flake is selected from pure iron, silicon steel, a permalloy (an Fe-Ni alloy) and an iron/cobalt amorphous alloy.

21. An antenna for a transponder according to claim 20, wherein the soft magnetic material composing said flake is a cobalt amorphous alloy (Co-Fe-Ni-B-Si).

22. An antenna for a transponder according to claim 19, wherein said flake has a thickness of 30  $\mu\text{m}$  or less and a diameter of 50 to 2,000  $\mu\text{m}$ .

23. An antenna for a transponder according to claim 19, wherein said flake has a thickness of 10  $\mu\text{m}$  or less and a diameter of 100 to 1,000  $\mu\text{m}$ .

24. An antenna for a transponder according to claim 19, wherein said synthetic resin is selected from the group consisting of the thermoset resins, e.g. epoxy resins, phenol resins, urea resins, unsaturated polyester resins, diacrylphthalate resins, melamine resins, silicone resins, and polyurethane resins; and thermoplastic resins, e.g. polyethylene resins, polypropylene resins, vinyl chloride resins, fluoroplastics, methacrylate resins, polystyrene resins, AS resins, ABS resins, ABA resins, polycarbonate resins, polyacetal resins, and polyimide resins.

25. An antenna for a transponder according to claim 19, wherein the amount of said synthetic resin in the composite material is 3 to 50 weight%.

Q5  
- Cont

26. An antenna for a transponder according to claim 19, wherein said flake comprises a cobalt base amorphous alloy, said synthetic resin is an epoxy resin, and the amount of said synthetic resin in the composite material is 10 to 40 weight%.

27. An antenna for a transponder according to claim 19, wherein said magnetic core has a thickness of 0.3 to 2 mm, and a width and length of 100 mm or less, respectively.

28. An antenna for a transponder according to claim 19, wherein said magnetic core has a thickness of 0.3 to 1 mm, a width of 10 to 25 mm and a length of 60 to 80 mm.

Sub 606 29. An antenna for a transponder according to claim 19, wherein the diameter of the coil conductor is 100 to 200  $\mu\text{m}$ .

Sub 607 30. An antenna for a transponder according to claim 19, wherein said coil is wound on the magnetic core perpendicular to the longer side of the magnetic core.

Sub 607 31. An antenna for a transponder according to claim 19, wherein said antenna for a transponder is suitable to carry as an ID card, a commuter pass or a coupon ticket which operates at a frequency over 100 kHz.

32. A transponder comprising two plate antennas set forth in claim 19, and an air-core antenna composed of spirally wound conductor.

33. A transponder according to claim 32, wherein the axes of said two or three antennas are perpendicular to each other.

34. A transponder according to claim 32, wherein said two plate antennas are provided in the plate transponder so that the axes of said two antennas or coils are perpendicular to each other, and said air-core antenna composed of the spirally wound conductor is provided in the plate transponder so that the axis thereof is perpendicular to the transponder plate.

35. A transponder according to claim 32, wherein said antenna for a transponder is suitable to carry as an ID card, a commuter pass or a coupon ticket which operates at a frequency over 100 kHz.

Qdd 997

08/701457

# **ABSTRACT OF THE DISCLOSURE**

An antenna for a transponder comprises a magnetic core composed of layered amorphous metallic thin plates or composite plates of soft magnetic flakes and a synthetic resin, and a coil wound on the magnetic core. A transponder comprises two antennas set forth above, and a spiral antenna.

08/701457-082906

FIG. 1

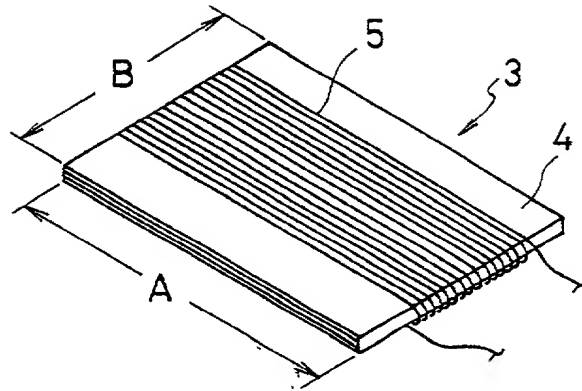


FIG. 2 A

PRIOR ART

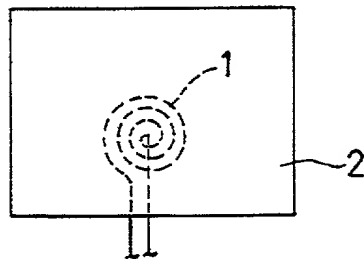


FIG. 2 B

PRIOR ART

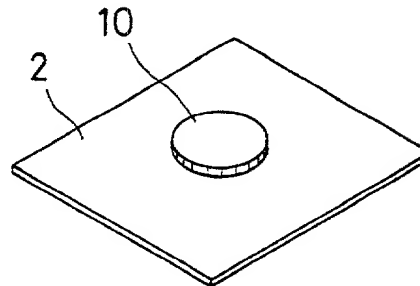


FIG. 3 A

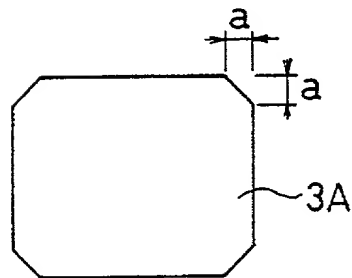


FIG. 3 B

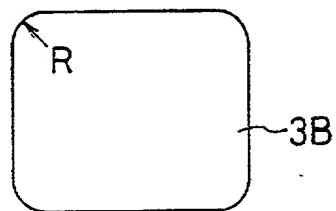


FIG. 4A

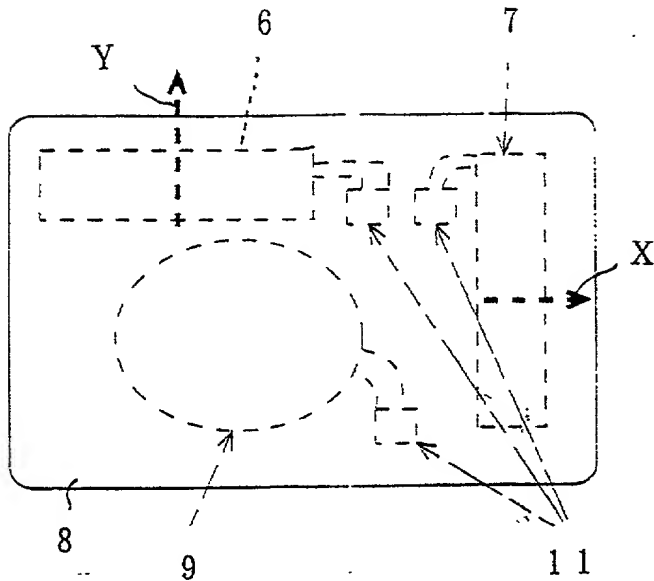
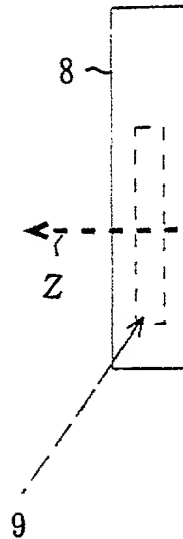


FIG. 4B



---> AXIS DIRECTION OF ANTENNA

FIG. 5A

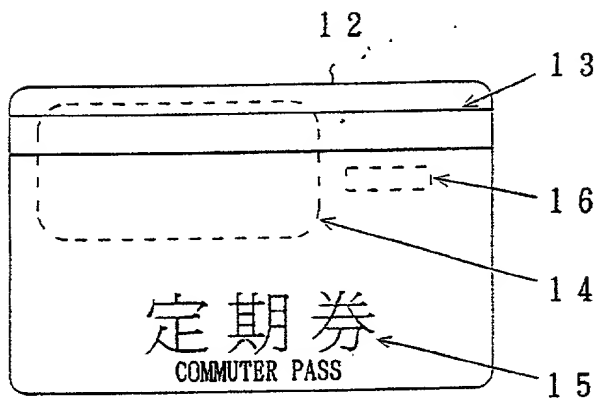


FIG. 5B

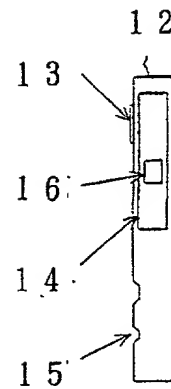


FIG. 6A

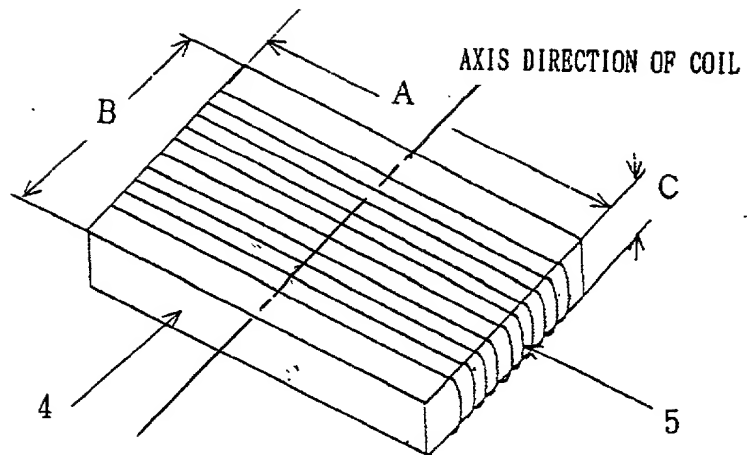
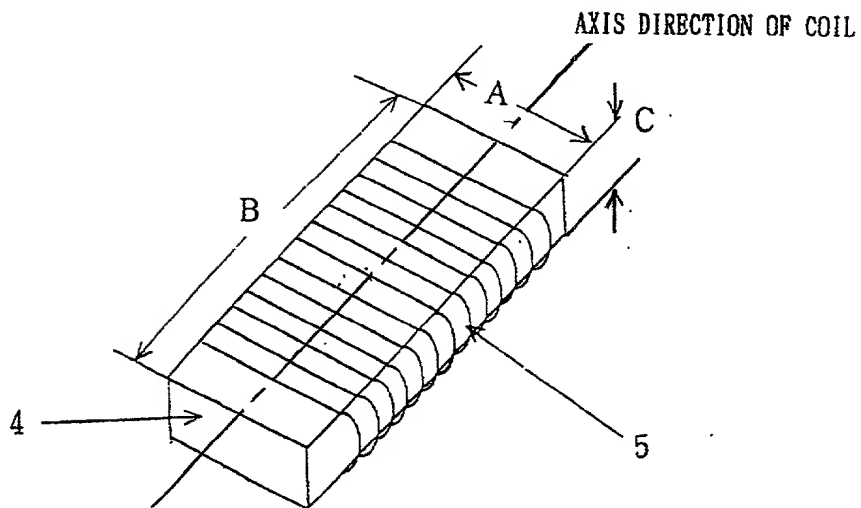
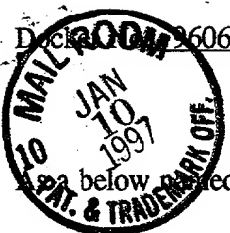


FIG. 6 B









DECLARATION FOR U.S. PATENT APPLICATION

I, the below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name.

I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled ANTENNA FOR TRANSPONDER AND TRANSPONDER the specification of which (check one of blocks 1, 2 or 3)

- 1. X is attached hereto.
- 2.      was filed on                      as International PCT Application Serial No.                      and was amended on                     . (if applicable)
- 3.      was filed on                      U.S. Application Serial No.                      and was amended on                     . (if applicable)

I hereby state that I have reviewed and understand the contents of the above-identified specification, including the claim(s), as amended by any amendment referred to above.

I acknowledge the duty to disclose information which is material to the examination of this application as defined in Title 37, Code of Federal Regulations, § 1.56.

I hereby claim foreign priority benefits under Title 35, United States Code, § 119 of any foreign application(s) for patent or inventor's certificate listed below and have also identified below any foreign application for patent or inventor's certificate having a filing date before that of the application for which priority is claimed.

<u>HEI 8-176543</u> (Number)	<u>Japan</u> (Country)	<u>05/07/96</u> (Day/Month/Year Filed)	Priority Claimed <u>X</u> Yes <u>  </u> No
<u>HEI 7-213353</u> (Number)	<u>Japan</u> (Country)	<u>22/08/95</u> (Day/Month/Year Filed)	<u>X</u> Yes <u>  </u> No
<u>HEI 8-176544</u> (Number)	<u>Japan</u> (Country)	<u>05/07/96</u> (Day/Month/Year Filed)	<u>X</u> Yes <u>  </u> No
<u>                    </u> (Number)	<u>                    </u> (Country)	<u>                    </u> (Day/Month/Year Filed)	<u>  </u> Yes <u>  </u> No

     See attached list for additional prior foreign applications

I hereby claim the benefit under Title 35, United States Code, § 120 of any United States application(s) listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States application in the manner provided by the first paragraph of Title 35, United States Code, § 112, I acknowledge the duty to disclose material information as defined in Title 37, Code of Federal Regulations, § 1.56 which occurred between the filing date of the prior application and the national or PCT international filing date of this application.

List Prior U.S. Applications:

(Appln. Serial No.) (Filing Date) (Status: Patented, Pending, Abandoned)

(Appln. Serial No.) (Filing Date) (Status: Patented, Pending, Abandoned)

(Appln. Serial No.) (Filing Date) (Status: Patented, Pending, Abandoned)

And I hereby appoint as principal Attorneys:

James E. Armstrong, III, Reg. No. 18,366; William F. Westerman, Reg. No. 29,988; Ken-Ichi Hattori, Reg. No. 32,861; John R. Pegan, Reg. No. 18,069; William G. Kratz, Jr., Reg. No. 22,631; Le-Nhung McLeland, Reg. No. 31,541; James P. Welch, Reg. No. 17,379; Ronald F. Naughton, Reg. No. 24,616; Albert Tockman, Reg. No. 19,722; Mel R. Quintos, Reg. No. 31,898; Michael J. Foycik, Jr., Reg. No. 30,928; Donald W. Hanson, Reg. No. 27,133; Stephen G. Adrian, Reg. No. 32,878; William L. Brooks, Reg. No. 34,129; Stephen B. Parker, Reg. No. 36,631; John F. Carney, Reg. No. 20,276; Edward F. Welsh, Reg. No. 22,455; Patrick D. Muir, Reg. No. 37,403; Gay A. Spahn, Reg. No. 34,978; and Theresa M. Stevens-Smith, Reg. No. 36,281.

Please direct all communications to the following address:

ARMSTRONG, WESTERMAN, HATTORI, McLELAND & NAUGHTON  
1725 K Street, N.W., Suite 1000-  
Washington, D.C. 20006  
TEL.: (202) 659-2930  
FAX: (202) 887-0357

I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under § 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

Full name of sole or first inventor Seiro YAHATA 1-00  
Inventor's signature Seiro YAHATA Date Sep. 11, 1996  
Residence Tokyo, Japan JPX  
Citizenship Japanese  
Post Office Address c/o Intellectual Property Service Corporation, 1-6-1, Ohtemachi, Chiyoda-ku, Tokyo, Japan

Full name of second joint inventor, if any Takanori ENDO 2-00  
Inventor's signature Takanori Endo Date September 11, 1996  
Residence Omiya-shi, Japan JPY  
Citizenship Japanese  
Post Office Address c/o Sohgo-kenkyusho, Mitsubishi Materials Corporation, 1-297, Kitabukuro-cho, Omiya-shi, Saitama-ken, Japan

Full name of third joint inventor, if any Masami MIYAKI 3-00  
Inventor's signature Masami Miyake Date September 11, 1996  
Residence Omiya-shi, Japan JPY  
Citizenship Japanese  
Post Office Address c/o Sohgo-kenkyusho Mitsubishi Materials Corporation, 1-297, Kitabukuro-cho, Omiya-shi, Saitama-ken, Japan

Full name of fourth joint inventor, if any Takashi TSUCHIDA 4-00  
Inventor's signature Takashi Tsuchida Date September 11, 1996  
Residence Omiya-shi, Japan JPY  
Citizenship Japanese  
Post Office Address c/o Sohgo-kenkyusho, Mitsubishi Materials Corporation, 1-297, Kitabukuro-cho, Omiya-shi, Saitama-ken, Japan

Full name of fifth joint inventor, if any \_\_\_\_\_  
Inventor's signature \_\_\_\_\_ Date \_\_\_\_\_  
Residence \_\_\_\_\_  
Citizenship \_\_\_\_\_  
Post Office Address \_\_\_\_\_

Full name of sixth joint inventor, if any \_\_\_\_\_  
Inventor's signature \_\_\_\_\_ Date \_\_\_\_\_  
Residence \_\_\_\_\_  
Citizenship \_\_\_\_\_  
Post Office Address \_\_\_\_\_

Full name of seventh joint inventor, if any \_\_\_\_\_  
Inventor's signature \_\_\_\_\_ Date \_\_\_\_\_  
Residence \_\_\_\_\_  
Citizenship \_\_\_\_\_  
Post Office Address \_\_\_\_\_

Full name of eighth joint inventor, if any \_\_\_\_\_  
Inventor's signature \_\_\_\_\_ Date \_\_\_\_\_  
Residence \_\_\_\_\_  
Citizenship \_\_\_\_\_  
Post Office Address \_\_\_\_\_